



MICROCOPY RESOLUTION TESTACHART

NATIONAL BUREAU OF STANDARDS 1965 A





TECHNICAL REPORT RD-RE-86-1

REAL-TIME PATTERN RECOGNITION USING A MODIFIED LIQUID CRYSTAL TELEVISION IN A COHERENT OPTICAL CORRELATOR

Don A. Gregory
Tracy D. Hudson
Research Directorate
Research, Development,
and Engineering Center



15 November 1985



U.S.ARMY MISSILE COMMAND

Redstone Arsenal, Alabama 35898-5000

Cleared for public release; distribution unlimited.

THE FILE COPY

84 - 12

DISPOSITION INSTRUCTIONS

DESTROY THIS REPORT WHEN IT IS NO LONGER NEEDED. DO NOT RETURN IT TO THE ORIGINATOR.

DISCLAIMER

THE FINDINGS IN THIS REPORT ARE NOT TO BE CONSTRUED AS AN OFFICIAL DEPARTMENT OF THE ARMY POSITION UNLESS SO DESIGNATED BY OTHER AUTHORIZED DOCUMENTS.

TRADE NAMES

USE OF TRADE NAMES OR MANUFACTURERS IN THIS REPORT DOES NOT CONSTITUTE AN OFFICIAL INDORSEMENT OR APPROVAL OF THE USE OF SUCH COMMERCIAL HARDWARE OR SOFTWARE.

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	. PECIPIENT'S CATALOG NUMBER
TR-RD-RE-86-1	AD-A168042	
4. TITLE (and Subtitle)	0	TYPE OF REPORT & PERIOD COVERED
REAL-TIME PATTERN RECOGNITION USING LIQUID CRYSTAL TELEVISION IN A CON-		Technical Report
CORRELATOR	ERENT OF ITORE	PERFORMING ORG. REPORT NUMBER
7. AUTHOR(a)		8. CONTRACT OR GRANT NUMBER(s)
	,	B. CONTRACT OR GRANT NUMBER(S)
Don A. Gregory Tracy D. Hudson	!	
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Commander, US Army Missile Command ATTN: AMSMI-RD-RE		
Redstone Arsenal, AL 35898-5248		
11. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE
Same as above		15 November 1985
		24
14. MONITORING AGENCY NAME & ADDRESS(If different	t from Controlling Office)	15. SECURITY CLASS. (of this report)
		UNCLASSIFIED
		154. DECLASSIFICATION DOWNGRADING SCHEDULE
		JONESOCE
16. DISTRIBUTION STATEMENT (of this Report)		
Cleared for public release; distri	bution unlimited	•
17. DISTRIBUTION STATEMENT (of the abstract entered	in Block 20, if different fro.	m Report)
	•	
18. SUPPLEMENTARY NOTES	······································	
19. KEY WORDS (Continue on reverse side if necessary as	nd Identify by block number)	
Liquid Crystal Television (LCTV)		
spatial light modulator real-time pattern recognition		
rear time pattern recognition		
20. ABSTRACT (Continue on reverse side if necessary on A commercially available flat		ystal Television (LCTV) has
heen slightly modified and used as a spatial light modulator in a Vander Lugt		
type coherent optical correlator. The small, (54 mm x 40.5 mm) inexpensive,		
(~\$100) LCTV was used as a replacement for extremely expensive modulators		
normally used in optical data processing such as the Hughes Liquid Crystal Ligh Valve and the Litton Magneto-Optic Device. Results show that the resolution,		
contrast, and speed of the LCTV in its present form, are sufficient for some		
basic real-time pattern recognition applications.		

DD FORM 1473 EDITION OF 1 NOV 65 IS OBSOLETE

UNCLASSIFIED

CONTENTS

		Page No
ı.	INTRODUCTION	1
ıı.	EXPERIMENTAL ARRANGEMENT	1
III.	EXPERIMENTAL RESULTS	2
IV.	CONCLUSIONS	3
REFER	ENCES	4

DTIC Unan	CRA&I TAB nounced ication	
By Dist. i	bution /	#************
	Availability C	odes
Dist	Avail and	or

Accesion For



al effective services harrings proposed agreem memories (services)

List of Illustrations

Figure		Page
1	Modified liquid crystal television	5
2	Pixel structure of the liquid crystal television	6
3	Experimental arrangement showing the location of the liquid crystal television (LCTV) and the prefiltering scheme	7
4	Optical Fourier transform of the pixel structure of the liquid crystal television	8
5	Tank model displayed on the liquid crystal television in Helium Neon laser light	9
6	Television monitor displaying the correlation signals due to the structure of the liquid crystal television, (upper bright spot), and the tank image, (lower bright spot)	10
7	Correlation intensity versus rotation of the input scene	11
8	Spatial distribution of the correlation signal as displayed on a standard television monitor	12

I. INTRODUCTION

The recent availability of inexpensive liquid crystal televisions (LCTV's) has led to experimenting with these devices as coherent spatial light modulators. The basic principle behind the operation of the LCTV is somewhat similar to that of the Hughes Liquid Crystal Light Valve (LCLV) which has been used for some time as an incoherent-to-coherent image converter in real-time pattern recognition systems (References 1 and 2). The 90° twisted nematic liquid crystal structure is common to both the LCTV and the transmission-type LCLV. A major difference in the two devices is the method of addressing. The LCLV is optically addressed (with coherent or incoherent light), while the LCTV must be electrically addressed. Both techniques have their advantages.

The second second

One such LCTV (Citizen, model 03TA-OA) has been modified by the removal of the poor quality parallel polarizers attached to both sides of the liquid crystal/electrode grid sandwich. The light diffuser was also removed and the screen hinge modified so that the screen could be positioned vertically as opposed to the designed, approximately 45°, viewing position. Figure 1 is a photograph showing the structural modifications made.

The electrode grid addressing structure (Figure 2) produces an array of 148 horizontal pixels by 122 vertical pixels. The pixel size is approximately 0.22 mm x 0.37 mm. The power consumption of the LCTV is 0.4 watts and can be operated on four AAA batteries for up to 10 hours. An AC adapter was also available for continuous operation. The dimensions of the LCTV, with the liquid crystal screen folded down, are 6.5 mm x 13.5 mm x 2.4 mm, and the weight is about 9 ounces including batteries.

The LCTV was observed to work reasonably well as a normal television set. The resolution was poorer than most standard televisions, but the grey levels and the TV frame rate speed of the device were reasonably acceptable to the eye.

II. EXPERIMENTAL ARRANGEMENT

The basic experimental setup is shown in Figure 3. This is the standard Vander Lugt optical correlator used in many optical data processing experiments — except for the addition of the LCTV (Reference 3). A prefiltering aperture was also included to remove the high spatial frequencies associated with the pixel grid structure of the LCTV. Figure 4 is a photograph of the optical Fourier transform of the unfiltered LCTV screen. The lens used to perform the transform has a focal length of 876 mm. It is obvious from this photograph that any matched filter made with the LCTV will be entirely dominated by the spectrum of the electrode grid structure. In order to minimize this effect, pinholes ranging in diameter from 0.5 mm to 1 mm were incorporated into a prefiltering arrangement. This proved to be quite effective in removing the higher spatial frequencies. Of course this technique may also remove higher frequencies contained in the image displayed on the LCTV. The combination of focal lengths and pinhole size can be chosen to minimize this problem. Initially, the focal lengths of L2, L3, and L4, shown in Figure 3, were chosen to be 178 mm, 200 mm, and 381 mm, respectively.

The LCTV was addressed using the video input plug provided on the device and a remote video camera. The standard television antenna also allowed the

option of RF addressing from an external transmitter. The LCTV may also be used as a monitor for most small computers. This allows computer-generated images to be used to make and/or address the Fourier transform matched filters.

III. EXPERIMENTAL RESULTS

Figure 5 is a photograph showing an example of the coherent images produced by the LCTV in HeNe laser light. The photograph was taken with the 1 mm prefiltering pinhole in the system. Adjusting the brightness control and the automatic gain control of the LCTV produced images in laser light having contrast ratios of 16 - 20 to 1. It was observed that the LCTV was not perfectly effective in rotating the polarization of the incident polarization by 90° (with no power or no image on the device). Regardless of the orientation of the incident polarization and the analyzer, a perfect null in the intensity transmitted by the analyzer could not be found. This may be due to some of the mass construction techniques used in producing the LCTV or perhaps a local distortion of the liquid crystal layer near the electrode grid structure elements. This effect caused the contrast ratio in the coherent image to be considerably lower than images produced by the other light modulators mentioned previously. The observed LCTV contrast ratio was, however, adequate for the experiments performed in this initial study.

The matched filters were made using well-established techniques (Reference 4). The holographic plates (Kodak 649F) were exposed to the filtered Fourier transform of the coherent LCTV image and a reference beam derived from the original collimated laser output. The reference-to-object beam ratio was varied so as to produce the highest diffraction efficiency for the low spatial frequencies contained in the image. The intensity of the reference beam was varied using a pair of crossed polarizers to obtain the desired beam ratio. The exposure times were chosen between 0.25 and 1.5 seconds.

An interesting problem was observed during the course of this investigation. For any pinhole/beam ratio/exposure time combination tested, the correlation signal detected by the CCD television camera shown in Figure 3, was composed of two intensities superimposed. It was found that one of the signals was due to the LCTV screen structure and the other due to the scene being displayed on the LCTV. This was determined by translating the input scene. The signal corresponding to the scene moved on the television monitor which was used to observe the correlation signals. This is a well known property of this type of optical correlator (Reference 5). The signal corresponding to the LCTV structure did not move (see Figure 6). This phenomena has been observed in work with a holographic lens used as the Fourier transform lens (Reference 6). Structure within the hololens produced a background correlation signal very similar to that observed in this report. Figure 7 illustrates the relative intensities of these two signals for a typical correlation. The input scene was a scale model of an M48 tank. The background signal remained reasonably constant regardless of the variations made in the input scene and the correlation signal due to the scene was always highly visible above the background as the input scene was rotated. The quantity of background signal was strongly dependent upon the focal length of the lens and the diameter of the pinhole used in the prefiltering arrangement. Figure 7 also illustrates the normal loss in scene correlation signal as the input scene was

rotated. The correlation signals due to the scene and the LCTV were super-imposed. The width of the correlation curve was somewhat larger than that obtained using a LCLV in the correlator and a similar input image. This was likely due to the lower resolution of the LCTV. The spatial distribution of the correlation signal is given in Figure 8. This data was taken using the TV line sweep capability of the Colorado Video image digitizer.

IV. CONCLUSIONS

CANALAN AND PROPERTY OF THE PR

In this initial investigation, it has been shown that small, inexpensive, liquid crystal televisions may be used as spatial light modulators in some real-time optical correlation applications. The LCTV used in this research was modified by the removal of the original polarizers used on the device. These polarizers were replaced with external, high quality polarizers, and it was found that the contrast of the resulting coherent (HeNe laser) image was greatly improved. This improvement in contrast was enough to investigate the possibility of using the LCTV as a real-time spatial light modulator. Inital results presented in the report show that the LCTV performs reasonably well in a standard coherent optical correlator and that the device deserves a much closer examination so that its operating parameters, such as resolution, contrast, and speed may be optimized for general optical data processing needs.

REFERENCES

- 1. Duthie, J. G. and Upatnieks, Juris, "Compact Real-Time Coherent Optical Correlators", Opt. Engr. 23, 007 (1984).
- 2. Liu, H. K. and Duthie, J. G., "Real-Time Screen Aided Multiple Image Optical Holographic Matched Filter Correlator", Appl. Opt. 21, 3278 (1982).
- 3. Goodman, J., Introduction to Fourier Optics, (McGraw-Hill, New York, 1968), p. 171.
- 4. Shulman, A., Optical Data Processing, (Wiley and Sons, New York, 1970), p.549.
- 5. Gaskill, J., Linear Systems, Fourier Transforms and Optics, (Wiley and Sons, New York, 1978), p. 334.
- 6. Gregory, Don A. and Liu, H. K., "Large Memory Real-Time Multichannel Multiplexed Pattern Recognition", Appl. Opt. 23, 4560 (1984).

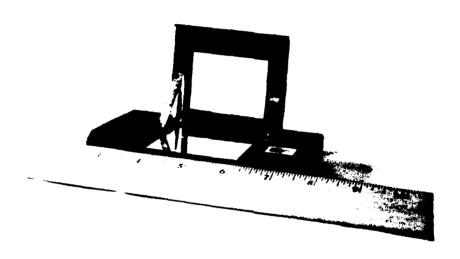
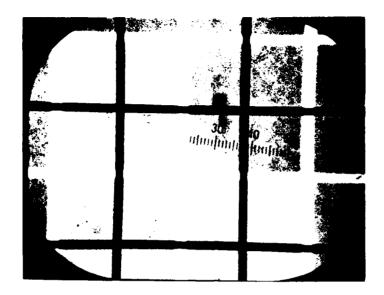


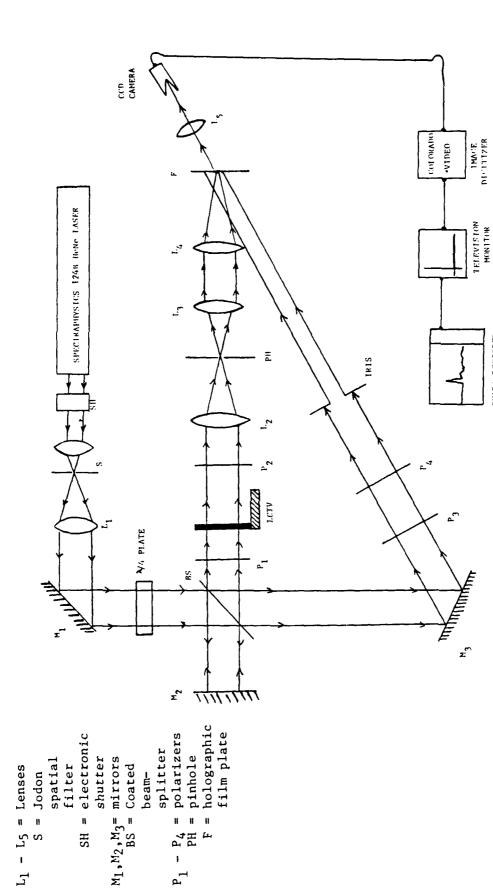
Figure 1. Modified liquid crystal television.



NOTE: This photograph was made before the external polarizers were removed and while an image was being displayed on the screen.

Figure 2. Pixel structure of the liquid crystal television.

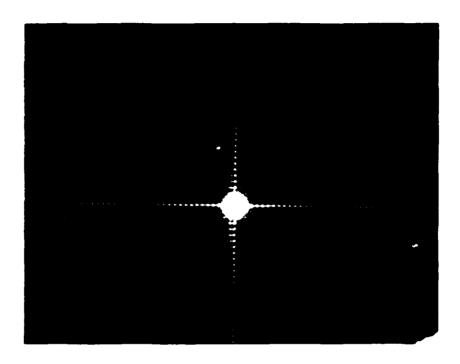
Paradamina Personal Reservation of the Paradaminant



Experimental arrangement showing the location of the liquid crystal television (LCTV) and the prefiltering scheme. Figure 3.

CHART RECORDER

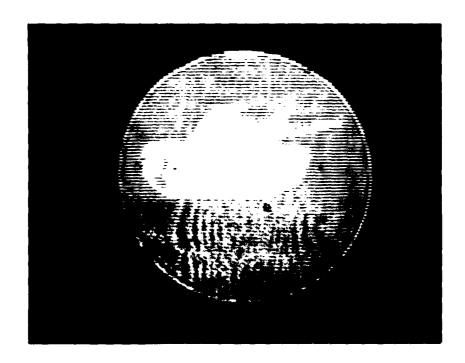
д Т



terrendra societa accepta especial appropria possible societa

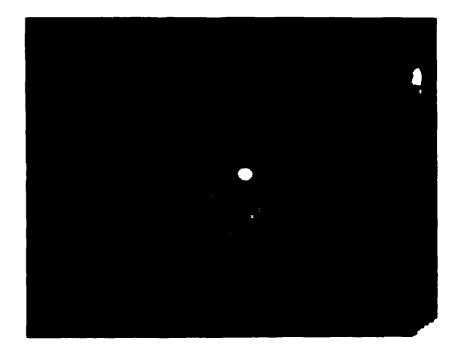
NOTE: The transform lens used for this photograph had a focal length of 876 mm.

Figure 4. Optical Fourier transform of the pixel structure of the liquid crystal television.



NOTE: The image has been prefiltered by the arrangement shown in Figure 3 using a 1 mm diameter pinhole.

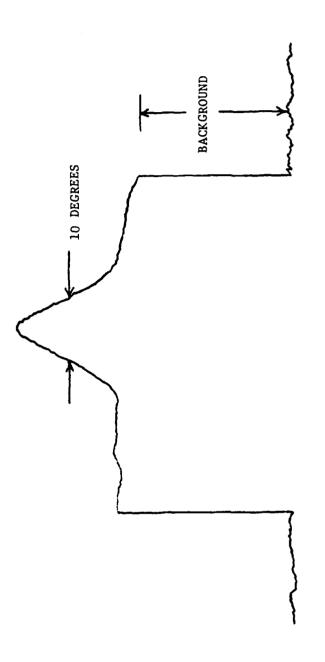
Figure 5. Tank model displayed on the liquid crystal television in Helium Neon laser light.



ALCOSONO REPRESENT FORESTA RESERVANT PERSONAL PROPERTY PROPERTY PROPERTY PROPERTY

NOTE: The two signals were separated by translating the tank model. A 0.5 mm diameter pinhole was used as a prefilter.

Figure 6. Television monitor displaying the correlation signals due to the structure of the liquid crystal television, (upper bright spot), and the tank image, (lower bright spot).



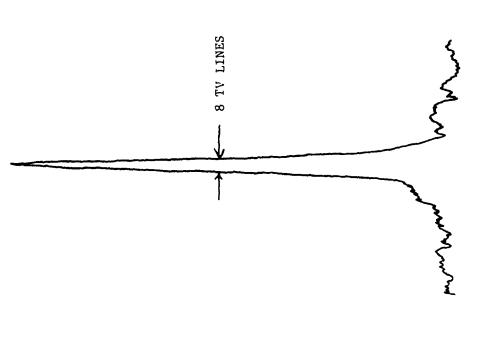
2222

and a second second seconds

This data shows the background intensity due to the structure of the liquid crystal television. This background can be decreased somewhat by using a smaller pinhole in the prefiltering arrangement showm in Figure 3. A 1 mm diameter pinhole was used in obtaining the data above. NOTE:

Figure 7. Correlation intensity versus rotation of the input scene.

125



The scene and background signals have been separated as in Figure 6. The above data is for the scene correlation only. The input scene used was a scale model of an M48 tank. NOTE:

Figure 8. Spatial distribution of the correlation signal as displayed on a standard television monitor.

	No. of Copies
Commander US Army Research Office ATTN: AMXRO-PH, Dr. R. Lontz PO Box 12211 Research Triangle Park, NC 27709	5
US Army Research and Standardization Group (Europe) ATTN: AMXSN-E-RX, LTC D. R. Reinhard Box 65 FPO New York 09510	1
Commander US Army Materiel Development and Readiness Command ATTN: Dr. James Bender Dr. Gordon Bushey 5001 Eisenhower Avenue Alexandria, VA 22333	1 1
Headquarters, Department of the Army Office of the DCS for Research Development & Acquisition ATTN: DAMA-ARZ Room 3A474, The Pentagon Washington, DC 20301	1
OUSDR&E Room 3D1079, The Pentagon Washington, DC 20301	1
Director Defense Advanced Research Projects Agency 1400 Wilson Boulevard Arlington, VA 22209	1
OUSDR&E ATTN: Dr. G. Gamota Deputy Assistant for Research (Research in Advanced Technology) Room 3D1067, The Pentagon Washington, DC 20301	1
Director of Defense Research and Engineering Engineering Technology Washington, DC 20301	1

	No. of Copies
Director Defense Advanced Research Projects Agency/STO	
ATTN: Commander T. F. Weiner D. W. Waish	1 1
1400 Wilson Boulevar Arlington, VA 22209	
Commander US Army Aviation Systems Command	1
12th and Spruce Streets St. Louis, MO 63166	•
Director US Army Air Mobility Research & Development Laboratory	1
Ames Research Center Moffett Field, CA 94035	•
Commander US Army Electronics Research & Development Command	
ATTN: AMSEL-TL-T, Dr. Jacobs DELEW-R, Henry E. Sonntag	1
Fort Monmouth, NJ 07703	•
Director US Army Night Vision Laboratory	
ATTN: John Johnson John Deline	1
Peter VanAtta Fort Belvoir, VA 22060	ī
Commander	1
US Army Picatinny Arsenal Dover, NJ 07801	1
Commander	1
US Army Harry Diamond Laboratories 2800 Powder Mill Road	•
Adelphi, MD 20783	
Commander US Army Foreign Science and Technology Center	
ATTN: W. S. Alcott	1
Federal Office Building	
220 7th Street, NE	

	No. of Copies
Commander US Army Training and Doctrine Command Fort Monroe, VA 22351	1
Director Ballistic Missile Defense Advanced Technology Center	
ATTN ATC-D ATC-O ATC-R	1 1 1
ATC-T PO Box 1500 Huntsville, AL 35808	1
Commander US Naval Air Systems Command Missile Guidance and Control Branch Washington, DC 20360	1
Chief of Naval Research Department of the Navy Washington, DC 20301	1
Commander US Naval Air Development Center Warminster, PA 18974	1
Commander, US Naval Ocean Systems Center Code 6003, Dr. Harper Whitehouse San Diego, CA 92152	1
Director, Naval Research Laboratory ATTN: Dave Ringwolt Code 5570, T. Gialborinzi Washington, DC 20390	1
Commander, Rome Air Development Center US Air Force ATTN: James Wasielewski, IRRC Griffiss Air Force Base, NY 13440	1
Commander, US Air Force, AFORSR/NE ATTN: Dr. J. A. Neff Building 410, Bolling Air Force Base Washington, DC 20332	1

	No. of Copies
Dr. David Cassasent Carnegie Mellon University Hamerschage Hall, Room 106 Pittsburg, PA 15213	1
Professor Anil K. Jain Department of Electrical Engineering University of California, Davis Davis, CA 95616	1
Terry Turpin Department of Defense 9800 Savage Road Fort George G. Meade, MD 20755	1
Dr. Stuart A. Collins Electrical Engineering Department Ohio State University 1320 Kennear Road Columbus, OH 43212	1
US Army Materiel Systems Analysis Activity ATTN: AMXSY-MP Aberdeen Proving Ground, MD 21005	1
US Army Night Vision Laboratory ATTN: DELNV-L, Dr. R. Buser Ft. Belvoir, VA 22060	1
Dr. F. T. S. Yu Penn State University Department of Electrical Engineering University Park, PA 16802	1
Dr. William P. Bleha Liquid Crystal Light Valve Devices Highes Aircraft Company 6155 El Camino Carlsbad, CA 92008	1

	No. of Copies
Commander, AFATL/LMT ATTN: Charles Warren Eglin Air Force Base, FL 32544	1
Environmental Research Institute of Michigan Radar and Optics Division ATTN: Dr. A. Kozma Dr. C. C. Aleksoff Juris Upatnieks PO Box 8618 Ann Arbor, MI 41807	1 1 1
ITT Research Intitute ATTN: GACIAC 10 West 35th Street Chicago, IL 60616	1
Dr. J. G. Castle 9801 San Gabriel, NE Albuquerque, NM 87111	1
Commander, Center for Naval Analyses ATTN: Document Control 1401 Wilson Boulevard	1
Arlington, VA 22209 Dr. J. W. Goodman Information Systems Laboratory Department of Electrical Engineering Stanford University Stanford, CA 04305	1
Eric G. Johnson, Jr. National Bureau of Standards 325 S. Broadway Boulder, CO '80302	1
Dr. Nicholas George The Institute of Optics University of Rochester Rochester, NY 14627	1
Naval Avionics Facility Indianapolis, IN 46218	1

	No. of
	Copies
AMSMI-RD, Dr. McCorkle	1
Dr. Rhoades	i
-RD-TI, Jerry Hagood	ĩ
-RD-AS, W. Pittman	î
-RD-GC, J. A. McLean	ī
-RD-RE, Dr. R. L. Hartman	1
Dr. J. S. Bennett	ī
Dr. J. G. Duthie	ī
Dr. D. A. Gregory	80
-RD-SS	1
-RD-CS-R, Reference	15
-RD-CS-T, Record Copy	1
-GC-IP, Mr. Bush	ī
AMCPM-PE-E, John Pettitt	1
-PE	;